

The Youngstown Business Incubator

the future rebooted

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1st Best University Affiliated

Incubator...

IN THE WORLD!

- University Business Incubator Index (UBII) in Stockholm, Sweden
- Youngstown State University







Outline

BUSINESS

YBI-Introduction

AM Overview

Applications

Cost/Economics

Additive Manufacturing Local Partners

- YBI
- Youngstown State University
- M7 Technologies
- RTI Titanium
- Applied Systems & Technology Transfer (AST2)















America Makes

National Additive Manufacturing Innovation Institute

Federal Funding From:

- Department of Defense
- Department of Energy
- NASA
- National Science Foundation
- National Institute of Standards and Technology





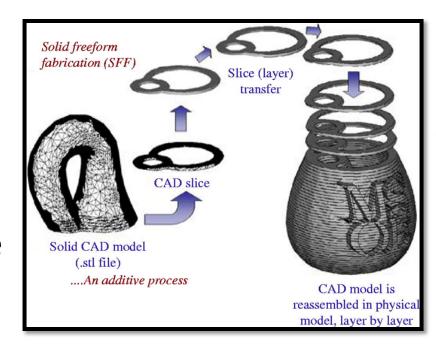






What is 3D Printing? (Additive Manufacturing)

- A method of creating an object by building it layer by layer on top of each other.
- Like the floors on a tall building.
- Additive process as oppose to traditional machining where material is removed



History of 3D Printing (RP)

1983 Charles Hull invents the Stereolithography Apparatus (SLA)

1984 Carl Deckard invents Selective Laser Sintering (SLS)

1986 the SLA is patented and 3D Systems is founded

1988 Scott Crump invents Fused Deposition Modeling (FDM)

1989 Stratasys is founded (FDM)

1989 EOS in Germany is founded (SLA and later on SLS)

1989 DTM Corp in founded and SLS is commercialized

1993 Three-Dimensional Printing (3DP) developed at MIT by Emanuel Sachs

1995 Z-Corp obtains exclusive license from MIT for the 3DP



From Polymers to Metals

EOS founded in 1989

- •SLS of polymers first
- •DMLS of metals in 1994
- Powder Bed Laser System

DTM introduced SLS 1992

- Polymer coated metal powder
- •Powder Bed Laser System
- •Acquired by 3D Systems in 2001

Concept Laser 2000

- Powder Bed Laser System
- •Full melting

Renishaw (former MTT UK)

- •Powder Bed Laser System
- •Development started in 1995

SLM Solutions (former MTT Germany 2000)

- Powder Bed Laser System
- •Development started in 1995

Phenix Systems (founded in 2000)

- •Powder Bed Laser System
- Recently Acquired by 3D Systems

LENS introduced 1995 by Sandia

- Only fully melted metals
- Powder Fed Laser System

EBM introduced by Arcam 2002

- Only fully melted metals
- Powder Bed Electron Beam System

Sciaky

- Only fully melted metals
- Wire Fed Electron Beam System
- Developed by NASA

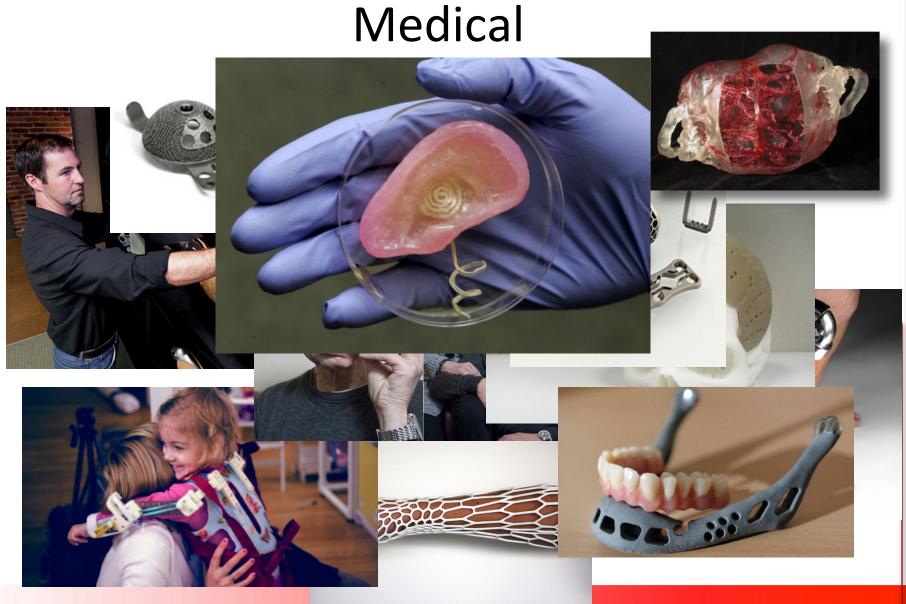
ExOne (founded in 2005)

- Powder Bed Printing System
- Post sintering and infiltration



RP to AM (3D Printing)





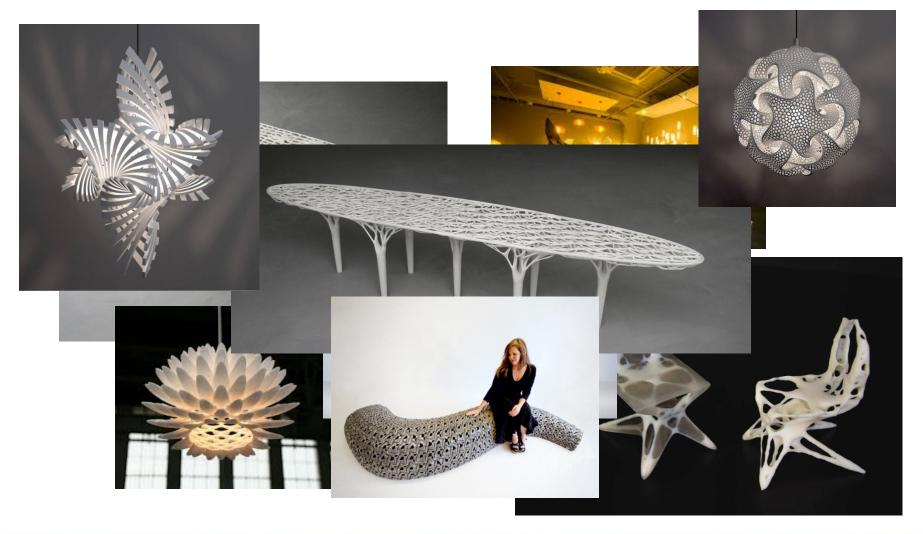
Aerospace



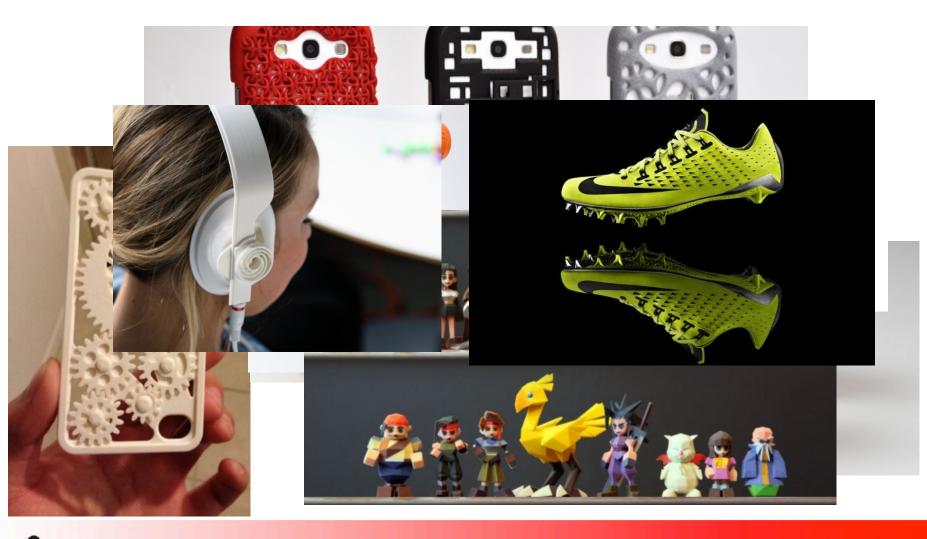
Architecture



Home and Decor

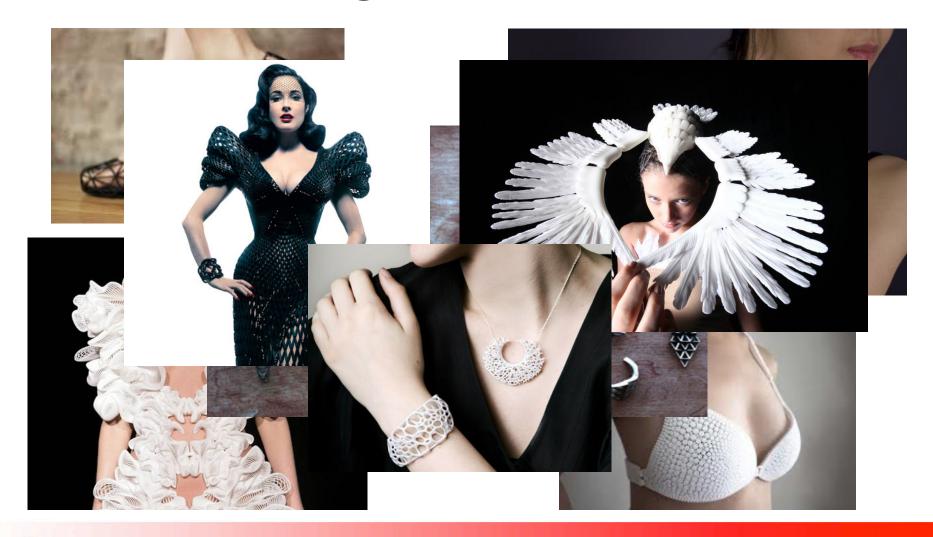


Consumer Products





Clothing and Accessories





Classification ASTM F2792-12a:

- Binder Jetting (Exone system)
- Directed Energy Deposition (LENS, EBF3)
- Material Extrusion (FDM)
- Powder Bed Fusion (EBM, DMLS)
- Sheet Lamination (Ultrasonic Consolidation and Mcorr)
- Vat Polymerization (SLA)



Binder Jetting

binder jetting, *n*—an additive manufacturing process in which a liquid bonding agent is selectively deposited to join powder materials.

- Materials: Metals, Ceramics and Sand
- Attributes:
 - Powders → Binding → Sintering
 - 'Processing' Temperature Independent
 - Porosity → Infiltration
 - e.g. Z-Corp, Ex-One



Binder Jetting

Powdered Metal: The re-coater applies a layer of powdered metal onto the build platform.

Bound Metal: The printhead selectively dispenses a proprietary resin onto the bed of powdered metal.

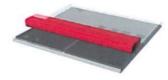
This process is repeated until the entire job is printed. The printed parts are then sintered in a vacuum furnace.

1. Binder print



The binder is selectively dispensed.

3. Next layer



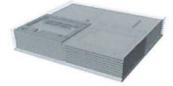
A new layer of powdered metal is spread.

2. New Layer



The build platform is lowered by a set increment.

4. Repeat



Steps 1-3 are repeated until the part is built.

5. Finishing



The unbound metal is removed, and the metal parts are sintered.



Directed Energy Deposition

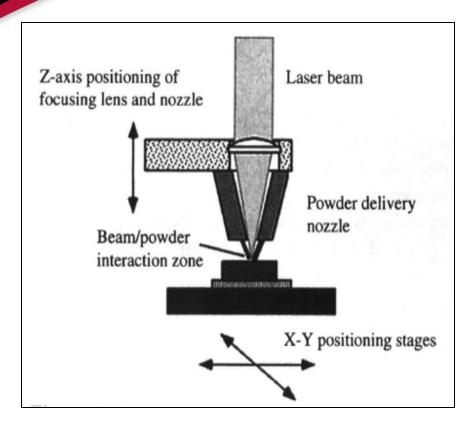
directed energy deposition, *n*—an additive manufacturing process in which focused thermal energy is used to fuse materials by melting as they are being deposited.

Discussion—"Focused thermal energy" means that an energy source (e.g., laser, electron beam, or plasma arc) is focused to melt the materials being deposited.

- Materials: Metals
- Source: Laser or Electron Beam
- Attributes:
 - Started from 'Cladding' operation
 - Powders → NC control → Melting
 - e.g. LENS, Sciaky



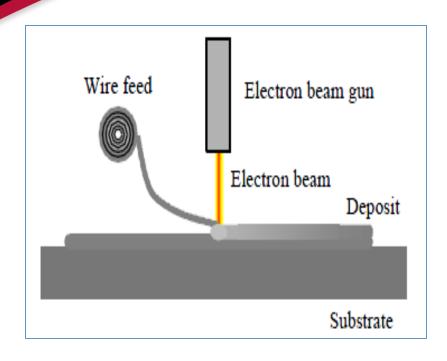
LENS



- Laser Engineered
 Net Shaping
- Ideal for Repairing
- Some 'Hybrid' processing
- 'Gradient' Materials
- Higher Deposition Rate



EBF³ - Sciaky



- Electron Beam
 Freeform Fabrication
- Wire-based
- Higher Deposition Rate
- Lower Resolution



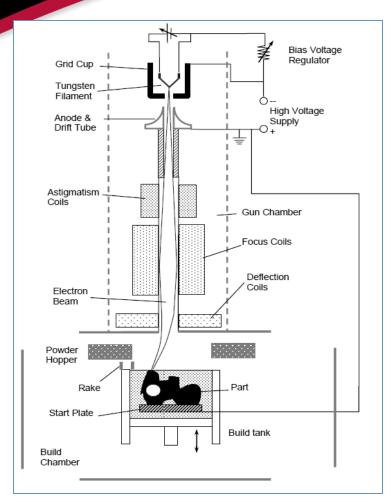
Powder Bed Fusion

powder bed fusion, *n*—an additive manufacturing process in which thermal energy selectively fuses regions of a powder bed.

- Materials: Metals and Plastics
- Source: Laser or Electron Beam
- Attributes:
 - Higher Density
 - Powders → Optics/EM control → Melting
 - Cold-bed vs. Hot-Bed process
 - e.g. EBM, DMLS

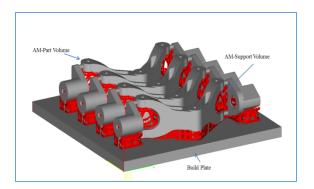


EBM - Arcam



https://www.youtube.com/watch?v=M_qSnjKN7f8

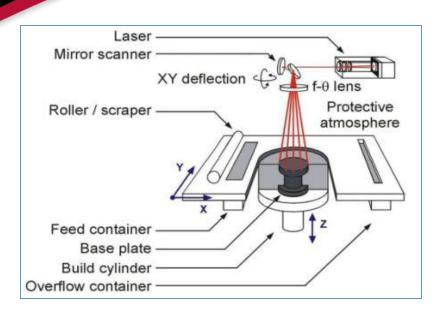
- Hot-Bed process
- Popular for Ti64
- Complete melting
- Pre-heating of bed
- Contour-Melt-Support
- In Vacuum







DMLS/EOS/SLM/Phenix



- Cold-Bed process
- Better resolution → EBM
- Parts at an angle to plate
- CoCr, SS are popular metals
- Stress-Relieving Annealing
- Inert gas atmosphere
- Scope for process modelling



Sheet Lamination

sheet lamination, *n*—an additive manufacturing process in which sheets of material are bonded to form an object.

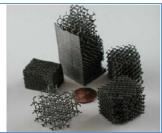
- Materials: Metals
- Solidica OEM
- Embedded Sensors applications
- Limited geometric freedom
- Lower production rate



Attributes of AM

- 'Freeform' Fabrication
 - Part design complexities
 - Eliminates expensive tooling
 - Fixture cost
 - Ideal for low-volume batch
 - Higher material utilization
 - Tough-to-process alloys
 - Non-homogeneity in cast ingots
- Poor surface finish
- Part feature inaccuracies
- Bonding of unprocessed powder
 - 'As-cast' surface textures
- Warping and Shrinkage during post-processing







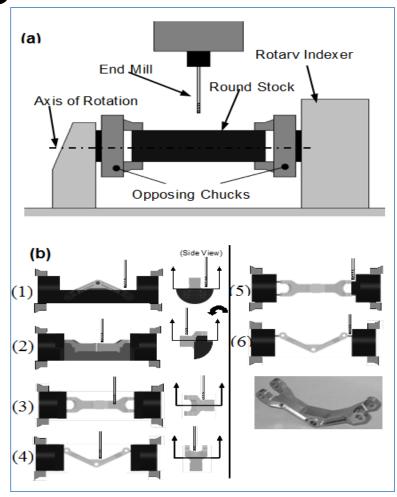
Takeaways

- Variety of Materials
- Variety of Applications
- Variety of Processing Technologies
- What are the <u>Challenges</u> in achieving complete 'Rapid Production'?



SM-Background

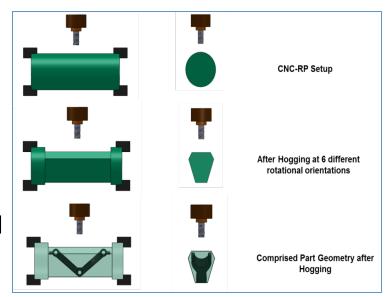
- CNC-RP
- 'CAD-to-produce' AM-like approach
- Layer-based island milling
- 4-axis CNC setup
- Sacrificial fixturing
 - Material and machining conditions → Deflection during machining
- Visibility analysis
 - Minimum amount of rotational indexing with maximum facet visibility





CNC-RP

- CNC-RP stages based on machining parameters and tooling:
 - Hogging
 - Roughing (featuredependent)
 - Finishing (featuredependent)
- Attributes of CNC-RP
 - Superior part accuracy and surface finish
 - Geometric limitations
 - Loss of material as scrap and chips
 - Machining of superalloys
 - Lower machinability
 - Tooling cost



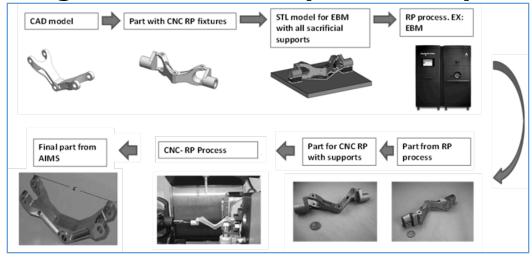
Hogging; Area-clearance



AIMS System Architecture

Incorporating CNC-RP fixtures prior to AM processing (e.g.

EBM)



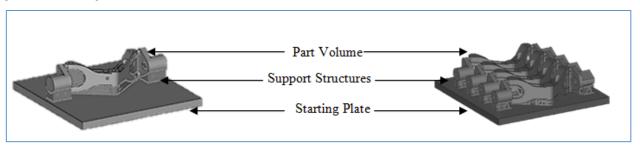
AIMS Process flow

- Part surface overgrowth for 'finish machining'
- Near-net AM part eliminates hogging and roughing (in CNC-RP)
- Single CAD file for entire process planning
- Two support structures:
 - Overhanging edges in AM
 - Fixturing supports for CNC-RP



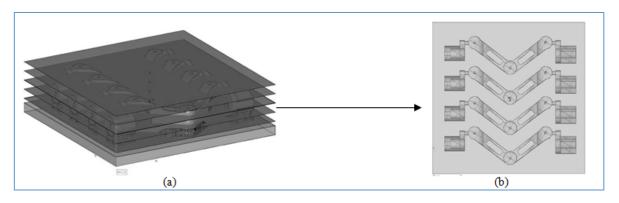
Case Study: Cost Model

Suspender part:



Low-volume Batch production

 Batch size considerations due to AIMS physical components → Build volume and Orientation



EBM Build Schematics



Economic Model- Cost factors

| Major Notations | Unit | Comments | | | | | |
|----------------------------|---------|--|--|--|--|--|--|
| iviajoi ivotations | Offic | | | | | | |
| General factors | | | | | | | |
| C _{unit} | \$ | Cost per unit | | | | | |
| Pv | mm³ | Part volume | | | | | |
| SPv | mm³ | Support volume- sacrificial supports | | | | | |
| C _{process} | \$/hr | Operating cost for each process | | | | | |
| C_{mat} | \$ | Cost of material in each process | | | | | |
| t _{build} | hr | Time to fabricate the part in additive process | | | | | |
| t _{setup_process} | hr | Setup time in each process | | | | | |
| t _{post_process} | hr | Post-processing time in each process | | | | | |
| CNC-RP specific factors | | | | | | | |
| Sv | mm³ | Volume of bar stock | | | | | |
| t _{hog} | hr | Time for hogging operation | | | | | |
| t _{rough} | hr | Time for roughing operation | | | | | |
| t_{finish} | hr | Time for finishing operation | | | | | |
| t_{tool_life} | hr | Cutting tool life duration | | | | | |
| t _{tool_change} | hr | Time for changing tool and tool set-up time | | | | | |
| | mm³ | Total volume removed at each stage in CNC-RP | | | | | |
| MRR | mm³/hr | Material Removal Rate at each stage in CNC-RP | | | | | |
| $C_{tooling}$ | \$/tool | Cost of cutting tools | | | | | |
| nt | | Number of tool changes in each stage | | | | | |
| $C_{tooling}$ | \$/tool | Cost of cutting tools | | | | | |
| | | EBM specific factors | | | | | |
| n _{EBM} | | Number of layers in EBM fabrication | | | | | |
| ρ | kg/mm³ | Density of metal powder used | | | | | |
| t _{FBM} | hr | Total build time in EBM | | | | | |
| t _{plate} | hr | Time to preheat the start plate to required temperature before fabrication | | | | | |
| t _{cool} | hr | Time to cool the build volume, retrieve part and recycle unused powder | | | | | |

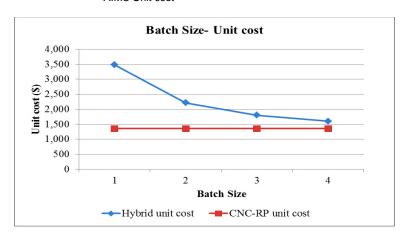


Case Study: Results

Breakdown of AIMS operation and tooling cost:

| | Hybrid Process | | | | | | | | |
|---------------|----------------|-----------------------|------------------|------------|---------------------|------------|-----------|--|--|
| Batch Size | EBM stage | | | CNC-RP | | Total Cost | Unit Cost | | |
| | Time (hrs) | Material Cost (\$) | EBM Cost (\$) | Time (hrs) | CNC-RP Cost (\$) | (\$) | (\$) | | |
| 1 | 28.03 | 104.23 | 3,019.54 | 10.38 | 359.50 | 3,483.27 | 3,483.27 | | |
| 2 | 33.98 | 138.97 | 3,672.93 | 20.76 | 619.00 | 4,430.90 | 2,215.45 | | |
| 3 | 39.93 | 185.30 | 4,337.91 | 31.14 | 878.50 | 5,401.71 | 1,800.57 | | |
| 4 | 45.88 | 247.07 | 5,018.32 | 41.52 | 1,138.00 | 6,403.39 | 1,600.85 | | |

AIMS Unit cost

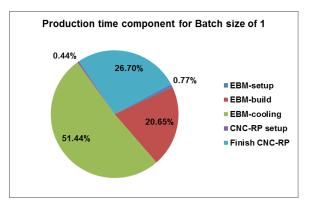


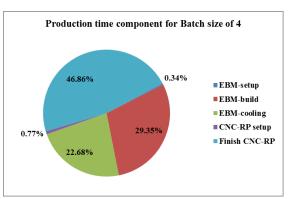
AIMS vs. CNC-RP Comparison



Case Study: Results

- No effect of batch size on CNC-RP
- Batch size reduces EBM and AIMS cost, due to amortized cooling and layer time





Time Components in AIMS



Case Study: Sensitivity Analysis

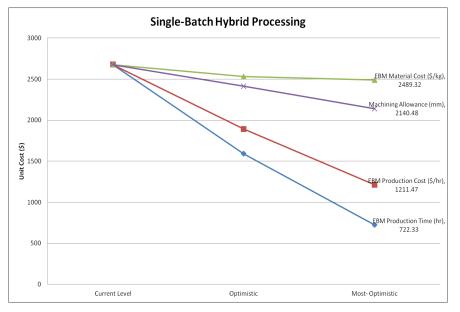
- Material cost: Aluminum vs. Inconel, atomization method, batch size, powder size, bar stock
- MRR: Machinability and part overgrowth
- Production time: EBM vs. DMLS vs. other AM technologies, Machining Ti64 vs. Al6065
- Production cost: Machining vs. AM technologies

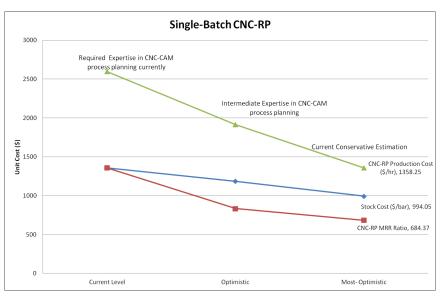
| Variables | Case- study- Section.3 | Level #2 | Level #3 |
|---------------------------------|------------------------------|----------|----------|
| EBM material cost (\$/kg) | 300 | 30 | 150 |
| CNC-RP stock cost (\$/unit) | 400 | 200 | 40 |
| Ratio: MRR/MRR-case study | 1 | 0.5 | 0.1 |
| EBM production time (hr/part) | 20 | 10 | 2 |
| EBM operating cost (\$/hr) | 104 | 66 | 33 |
| CNC-RP operating cost (\$/hr) | 25 | 50 | 75 |
| Finish machining allowance (mm) | 2.54 | 0.25 | 1.25 |



Case Study: Sensitivity Analysis

- CNC-RP benefits the most from increased MRR ratio
- Machining time influences more than stock cost
- Production time influences the most in AIMS (cooling)
- Lower production cost reduces the unit cost in AIMS
- Advantage of AIMS:
 - Machinability has smaller effect on unit price → Superalloys

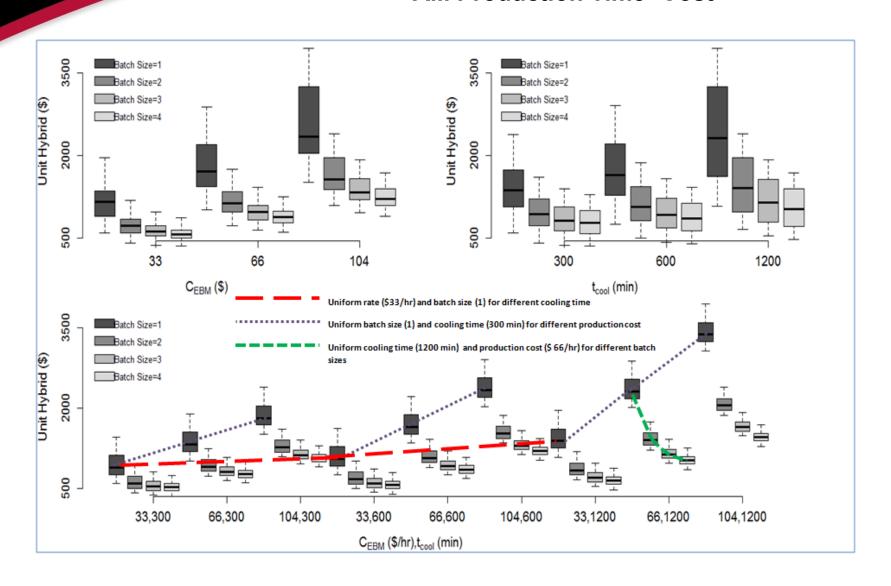




AIMS Unit cost CNC-RP Unit Cost



AM Production Time-Cost





Summary

- Removal of hogging and roughing is a major contribution along with CNC-RP based re-orientation hybrid method
- Operation cost of CNC machine is lower → preference to produce Aluminum or Brass through conventional methods
- AM (e.g. EBM) cooling or secondary production time is very critical cost component
- Material utilization → More expensive difficult-to-machine alloys



Summary

- Three-fold benefits:
 - Elimination of additional fixtures to AM
 - 'Finish' only CNC-RP leads to reduction in machining time and lower tooling cost
 - Higher material utilization through 'near-net' AM part approach
 - Batch production (Build volume, part design, build orientation constraints)
- · Criteria:

$$t_{pre-finishing} = t_{setup-CNC-RP} + t_{hog} + t_{rough}$$

$$C_{RoughStock} = (C_{machining} \times t_{pre-finishing}) + C_{tool(H)} + C_{tool(R)} + C_{CNC-RP-stock}$$

$$C_{RoughStock} \leq C_{EBM}$$

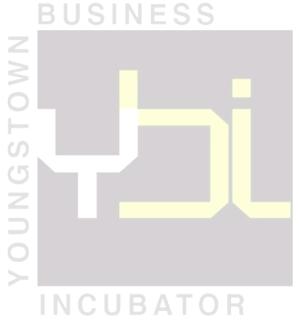


Contact

Questions!!

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Thank you!



the future re-booted

...questions?

Cost Models

Cost of AM unit is a function of material and production time

$$C_{unit} = C_{material} + (C_{add} \times t_{add})$$
 $t_{add} = t_{setup_add} + \sum_{i=1}^{n} (t_{build_i}) + t_{post_process}$

 Cost of CNC-RP unit is a function of material, tooling production time

$$C_{unit} = (S_v \times C_{mat_CNC-RP}) + (C_{CNC-RP} \times t_{CNC-RP}) + (C_{tooling} \times n_{stage})$$

$$t_{CNC-RP} = t_{setup_CNC-RP} + t_{hog} + t_{rough} + t_{finish}$$

$$n_{stage} = \frac{(\Delta V)}{MRR} \times \left(\frac{1}{t_{tool_life}}\right)$$

$$t_{stage} = \frac{(\Delta V)}{MRR} + (n_{stage} \times t_{tool_change})$$

AIMS Cost Model

• In this study, EBM is the AM component. Hence, the EBM build time can be detailed for each layer 'i':

$$\sum_{i=1}^{n} (t_{build_i}) = t_{plate} + t_{raking} + t_{pre\ heating} + t_{melt_i} + t_{support_i} + t_{post\ heating}$$

The melting and support time for each layer can be expressed as:

$$t_{melt_i} = \sum_{i=1}^{n} \left(\frac{Contour\ scan\ length}{Contour\ Speed} \right) + \sum_{i=1}^{n} \left(\frac{Melt\ scan\ length}{Melt\ Speed} \right)$$

$$t_{support_i} = \sum_{i=1}^{n} \left(\frac{Support\ scan\ length}{Support\ Speed} \right)$$

AIMS Cost Model

Hence, the EBM cost-component can be noted as:

$$t_{EBM} = t_{setup_EBM} + \sum_{i=1}^{n} (t_{build_i}) + t_{cool}$$
 $C_{EBM} = (\eta \times (P_v + SP_v) \times \rho \times C_{kg}) + (C_{EBM} \times t_{EBM})$

Including the finish CNC-RP component, AIMS unit cost is:

$$C_{Hybrid} = (C_{CNC-RP} \times (t_{setup_CNC-RP} + t_{finis\,h})) + (C_{tooling} \times n_{finis\,h}) + C_{EBM})$$

Cost-Model Parameters

- CNC-RP: (Ti-64)
 - Operating cost → \$ 25/hr
 - Stock setup time →10 minutes
 - Tool change → 10 minutes (including tool length qualification)
 - Cutting tools (four flute carbide flat end mills)
 - diameters of 25.40 mm, 6.35 mm and 3.18 mm for hogging, roughing and finishing respectively.
 - Machining parameters (surface speed of 508 mm/s)
 - Chip load of 0.05 mm in the case of hogging and roughing
 - Chip load 0.03 mm in the case of finishing.
 - Layer thickness (depth of cut) of 5.08 mm, 0.51 mm and 0.05mm in the case of hogging, roughing and finishing operation.
 - Stock volume → Diameter of 63.50 mm and a length of 203.20 mm and valued at \$ 400 per stock.
 - Average tool life was assumed to be 100 minutes of machining time and tooling cost of \$20/tool.

Cost-Model Parameters

- EBM: (Ti-64)
 - Operating cost → \$ 104/hr
 - Layer thickness → 0.07 mm
 - Setup and plate pre-heating time →90 minutes
 - EBM cost \rightarrow \$ 300/kg, 5 % loss in powder handling
 - Constant beam speed conditions
 - Effective contour speed → 17.18 mm/s
 - Support speed → 50 mm/s
 - Beam overlap → 0.20 mm
 - Each layer:
 - Raking duration → 10 seconds
 - Preheating → 12.5 seconds
 - Post-heating → 12.5 seconds
 - Melt beam speed → 500 mm/s
 - Cooling and part retrieval time → 480 minutes